

Two Level System Noise (TLS) and RF Readouts

Christopher McKenney

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Caltech



Two Level System (TLS) and Superconducting Resonators

Have well known effects in superconducting resonator applications

- Energy dissipation – limits Q's of devices (Q-bits, MKIDS, etc)
- Frequency shift – small shifts in resonant frequency
- Add Frequency Noise

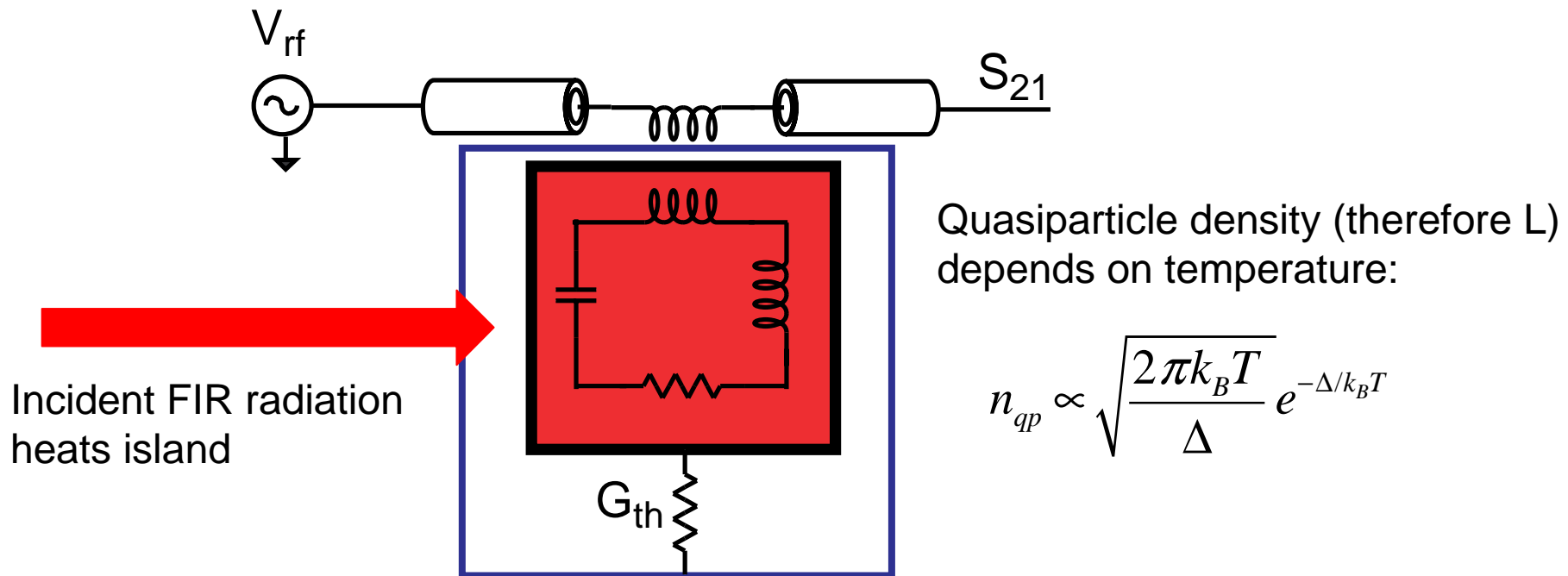
No clear theoretical understanding of noise

- Temperature power power dependence well mapped
- Limited exploration of variation with resonator frequency
- Some TLS physics suggest lower noise as $hf \ll kT$

Kinetic Inductance Thermometry And Radio-Frequency Readouts

Possible use of LC resonators at Kinetic Inductance Thermometers (KITs)

- FIR radiation absorbed by suspended bolometer island
- Temperature read out via RF-KIT
- RF - Require large capacitors with amorphous dielectrics (TLS noise)



Kinetic Inductance Thermometry And Radio-Frequency Readouts

TLS Noise - potentially limiting factor in this FIR detection scheme

Need TLS Noise < Photon Noise

$$S_{TLS} < \frac{\beta^2}{4Q_\sigma^2} \frac{1+n}{n\Delta\nu}$$

β – ratio of frequency to
dissipation response
 n – optical efficiency ~ 1
 $\Delta\nu$ – optical bandwidth

$$\beta = \frac{\delta\sigma_2}{\delta\sigma_1} \sim 1-10$$

Noise for a FIR spectrometer detector with typical values:

$$n = 1, \beta = 10, Q_i = 10^5, \Delta\nu = 0.3 \text{ GHz: } S_{TLS} < 2 \times 10^{-17} / \text{Hz}$$

Is this achievable with radio-frequency readouts?

Exploration of TLS effects at Radio-Frequency

Lumped LC resonators spanning wide frequency range

Inductance

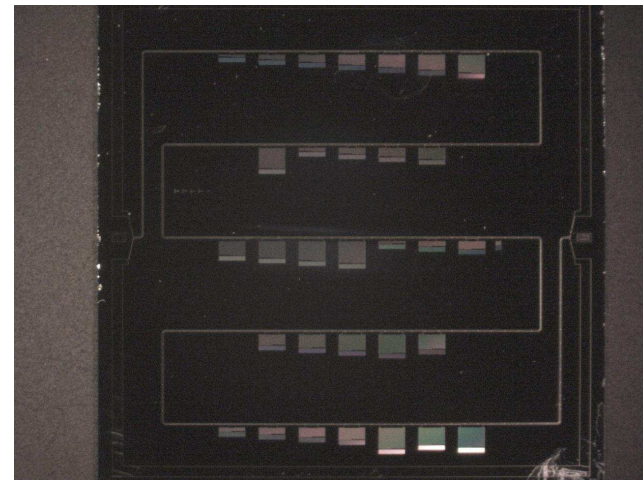
- High α materials – TiN, NbTiN
- Vary frequency of resonators by adjusting length of meander inductors

Capacitance – goals:

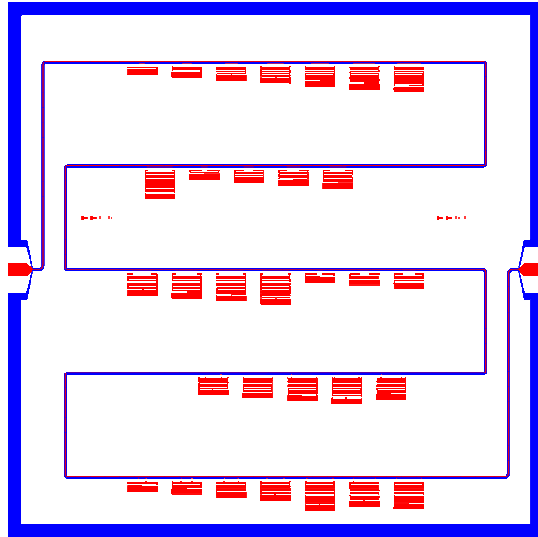
- Interdigitated Capacitors – 250 MHz – 3 GHz
- Parallel Plate – 50 MHz – 1 GHz
- Multiple dielectrics – SiO₂, SiN, Si, SOI

Fabricated our first device:

- **28 Resonators**
- **IDC, 250 MHz – 1 GHz**



Devices: Lumped LC resonators spanning wide frequency range



Device design:

31 Resonators

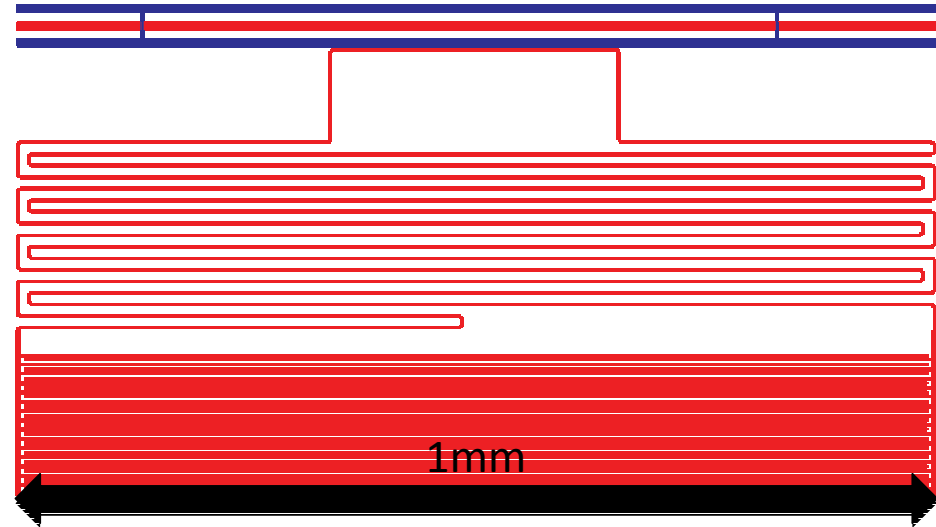
Resonator + CPW center conductor:

NbTiN ($T_c \sim 14$ K)

Ground Planes: Nb

Dielectric coating: 200nm SiO₂

Frequency: 250 MHz – 1 GHz



IDC:

Fingers 2 μ m wide, 2 μ m spacing

32 Fingers total (~ 160 μ m long)

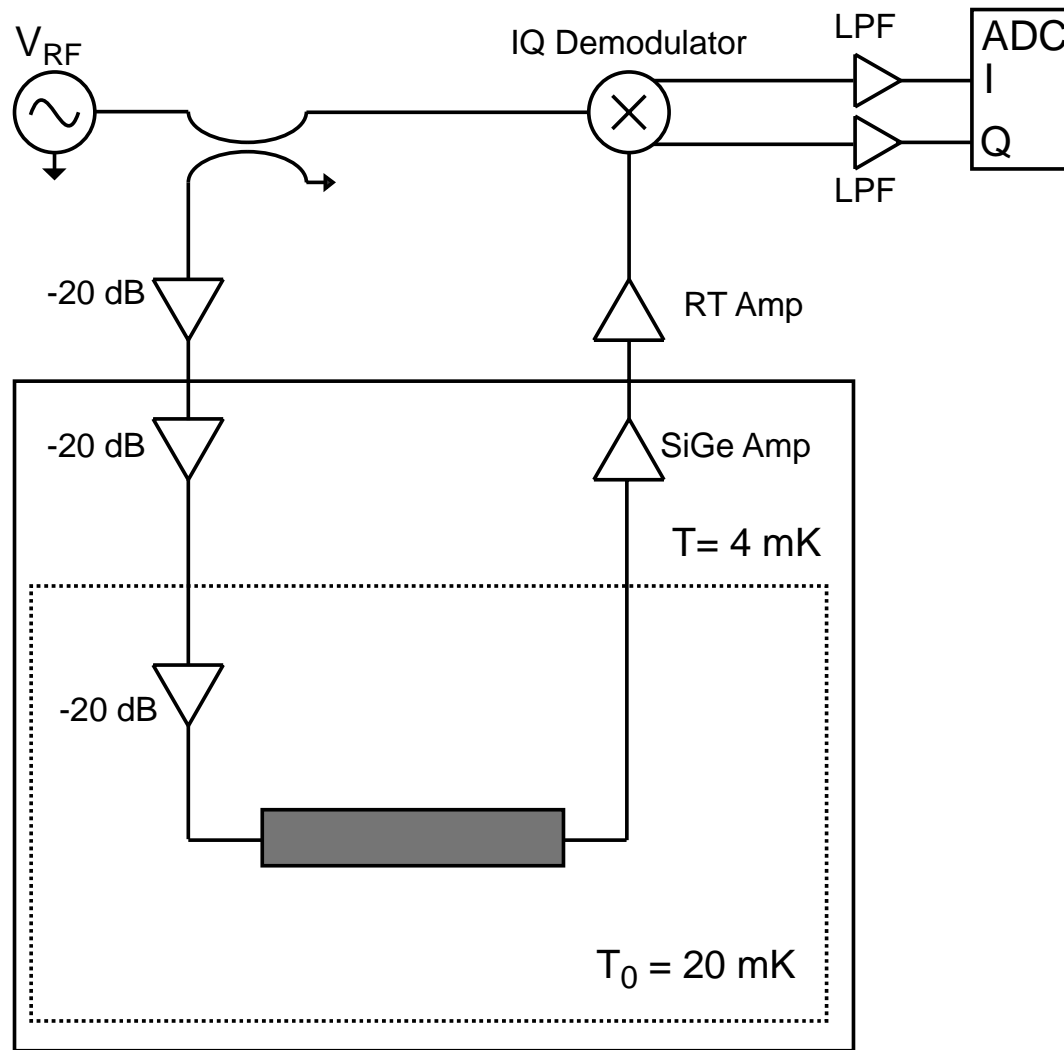
Finger length: 1mm

Capacitance ~ 2 pF

Inductor:

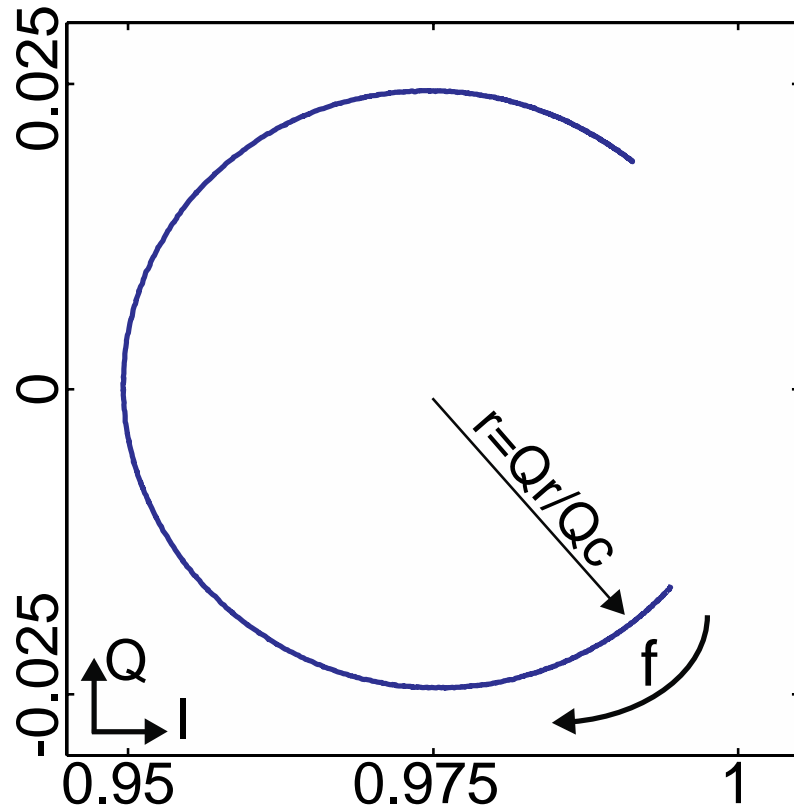
NbTiN ~ 6 pH / square

Probe devices by measuring forward transmission (S21)



Device response plots a circle in the IQ plane:

For the resonator with $f_{res} = 813$ MHz:



$$S_{21} = 1 - \frac{Q_r}{Q_c} \frac{1}{1 + 2i\delta x Q_r}$$

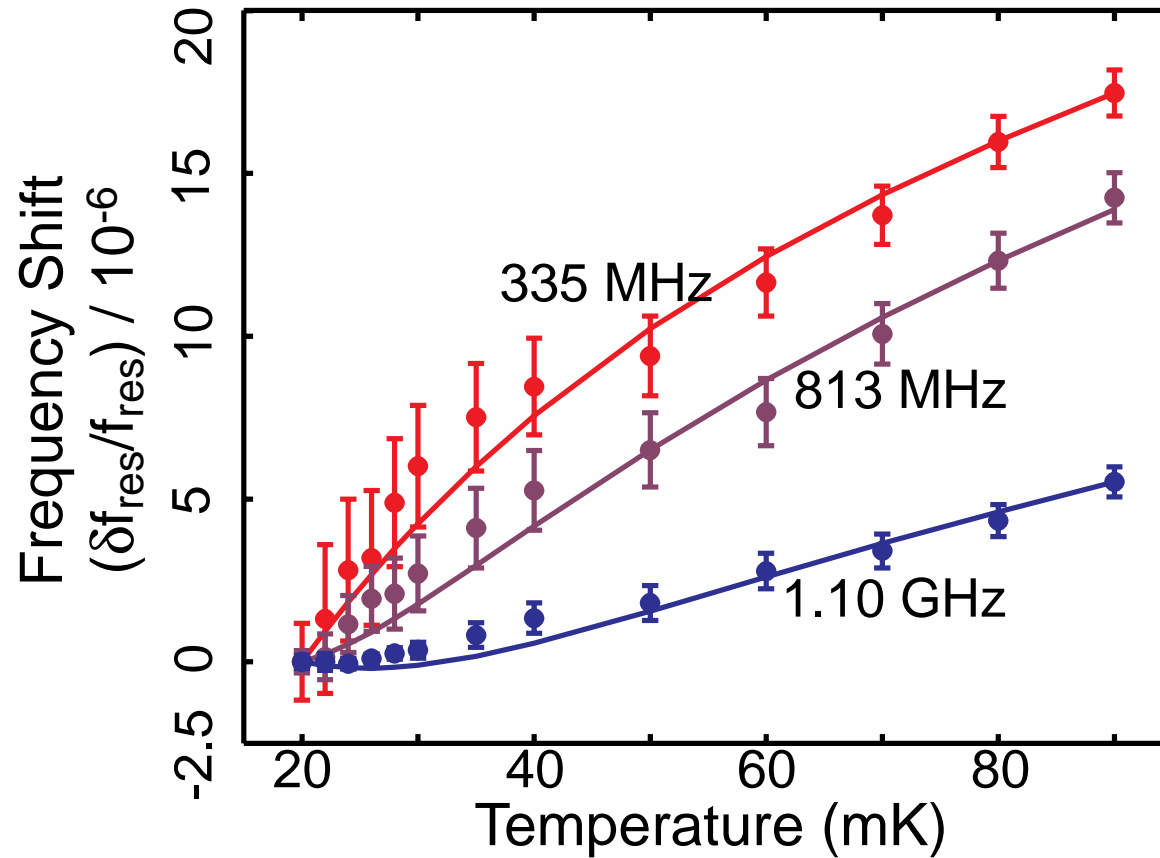
Fits yield:

$$Q_i = 1.0 \times 10^5$$

$$Q_c = 3.8 \times 10^6$$

Devices are undercoupled!

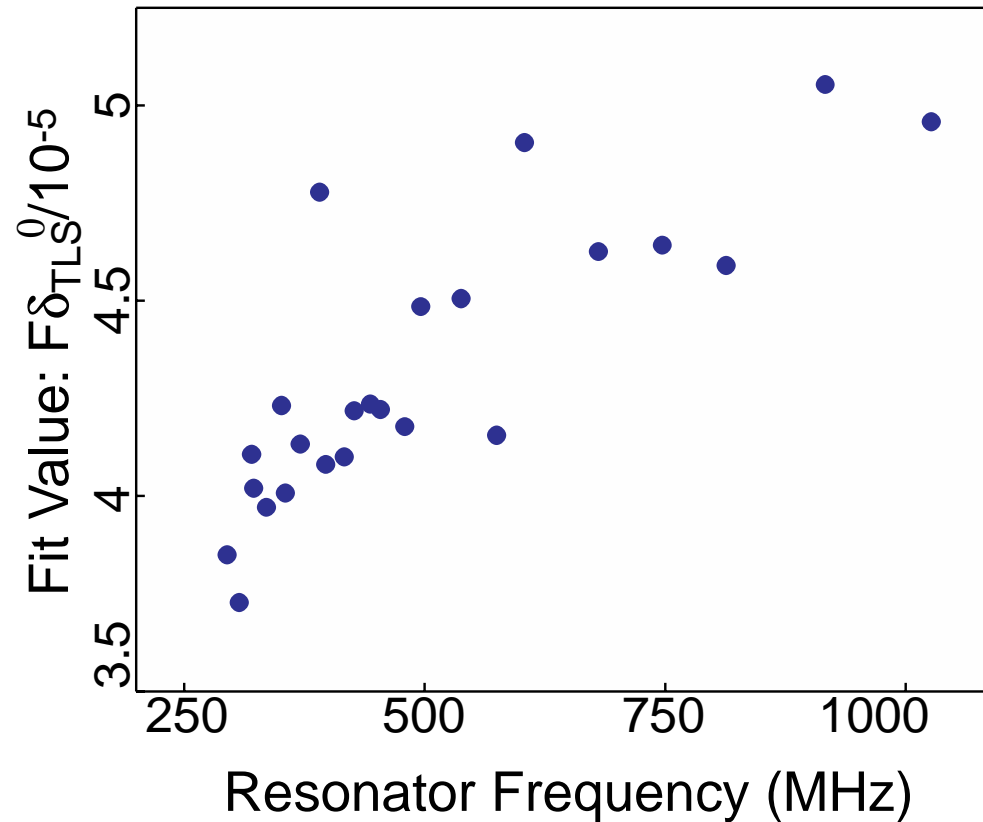
Shift in resonant frequency – Matches TLS predictions



Lines are fits to:

$$\frac{f_R - f_0}{f_0} = \frac{F \delta_{TLS}^0}{\pi} \left[\text{Re} \left(\frac{1}{2} - \frac{\hbar \omega}{2j\pi k_B T} \right) - \ln \left(\frac{\hbar \omega}{2k_B T} \right) \right]$$

Loss tangent fit over 28 resonators:

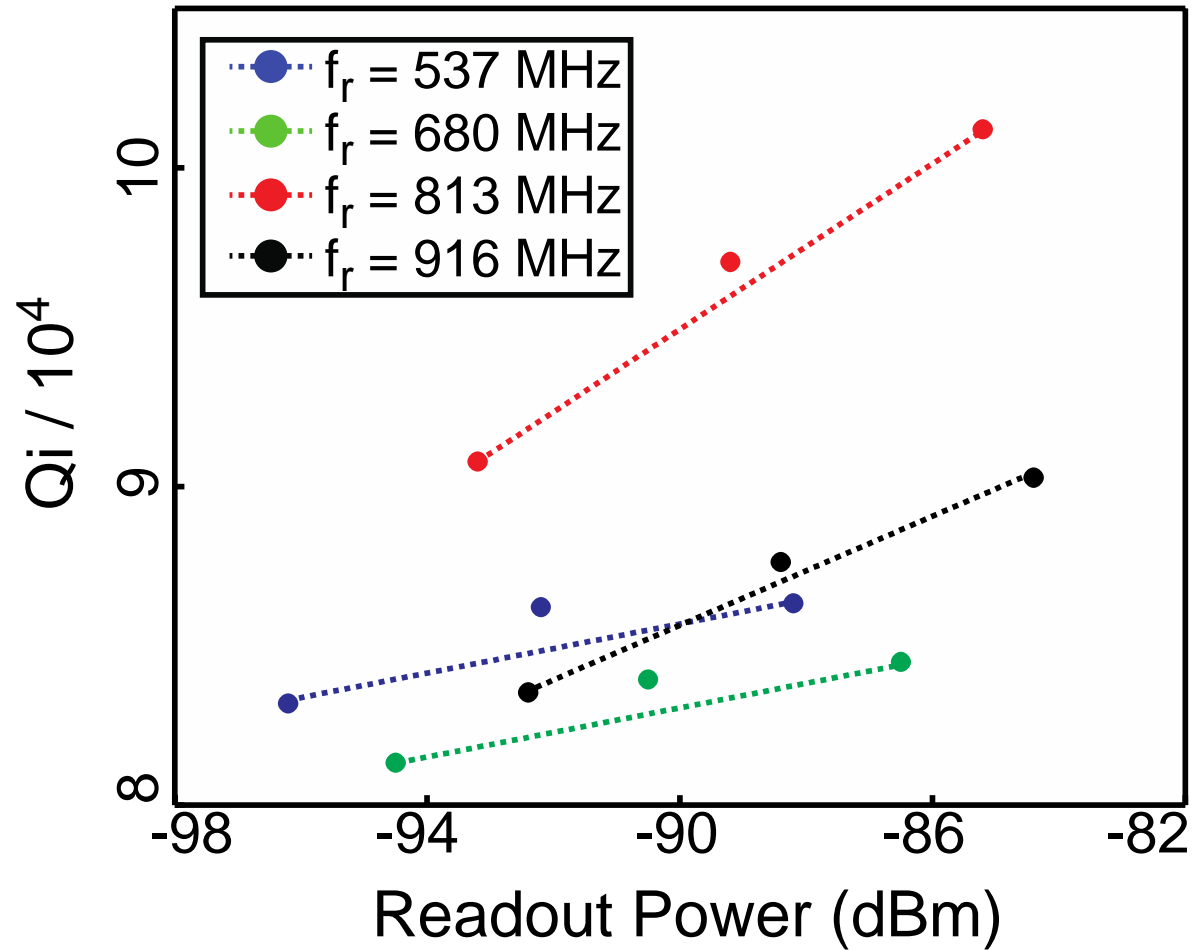


Very little change as frequency varies ~ 20%

Sonnet simulations indicate $F \sim 0.035$ for our geometry

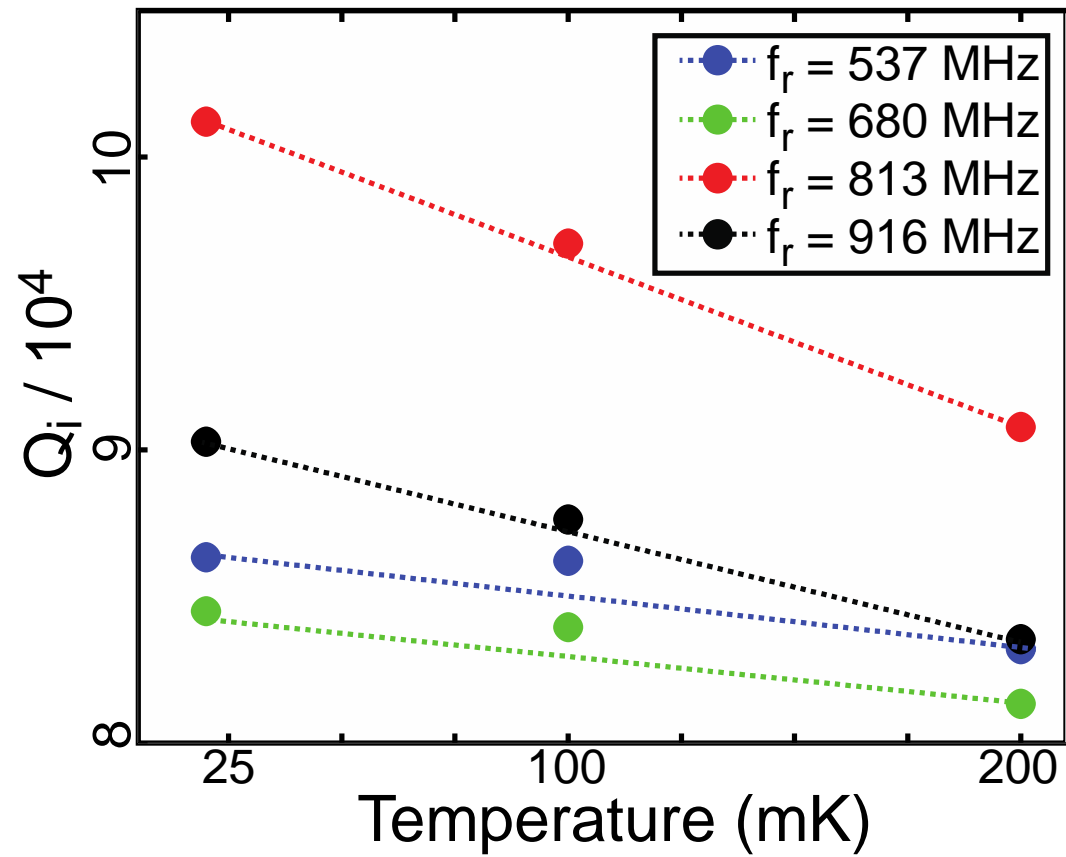
$Q_{\text{TLS}} \sim 800$ for this amorphous SiO₂

TLS saturates with increasing power – $T = 100$ mK



Observe decreasing Q_i with temperatures

Change in Q_i with temperature



Internal Qi depends strongly on electric field and temperature
Weak Fields – TLS saturates as temperature increases

$$\delta_{TLS} = \delta_{TLS}^0 \tanh\left(\frac{\hbar\omega}{2kT}\right)$$

Under Bloch model TLS saturation condition

$$\Omega^2 T_1 T_2 \gg 1$$

$$\Omega = \vec{d} \cdot \vec{E} / \hbar$$

$$\text{For SiO}_2 - E_{critical} \approx 2.6 \left(\frac{f}{\text{GHz}}\right)^{3/2} \coth^{1/2}\left(\frac{hf}{2kT}\right) \left(\frac{T}{200\text{mK}}\right)^{0.75}$$

4 GHz, 200 mK: $E_{crit} \sim 30$ V/m

500 MHz, 100mK: $E_{crit} \sim 1$ V/m

Our fields $\sim 10^3$ V/m, well above critical field

Internal Qi depends strongly on electric field and temperature
 Weak Fields – TLS saturates as temperature increases

$$\delta_{TLS} = \delta_{TLS}^0 \tanh\left(\frac{\hbar\omega}{2kT}\right) \longrightarrow \delta_{TLS}^0 \left(\frac{|\vec{E}|}{E_c}\right) = \frac{\delta_{TLS}^0 \tanh\left(\frac{\hbar\omega}{2kT}\right)}{\sqrt{1 - \left(\frac{|\vec{E}|}{E_c}\right)^2}}$$

Under Bloch model TLS saturation condition

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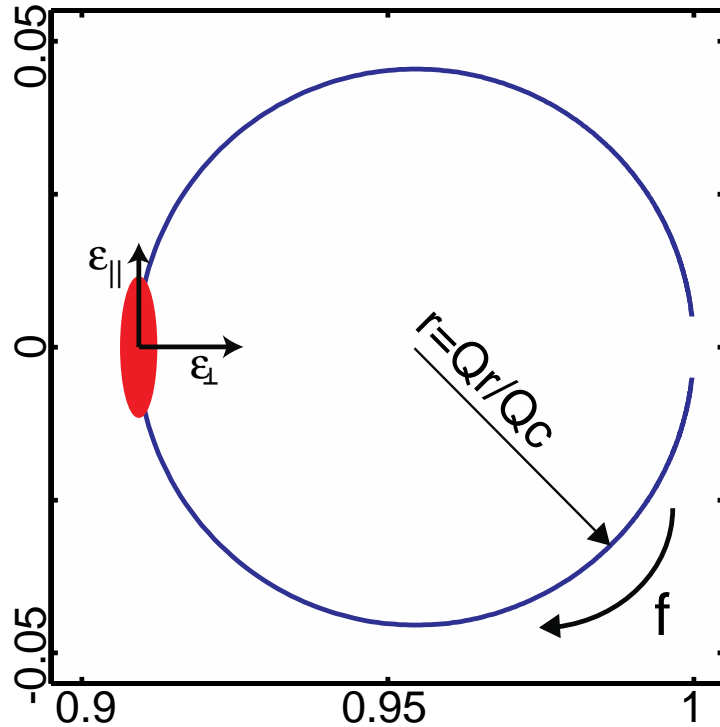
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Measure noise as S21 fluctuations

(I) Amplitude and Frequency (Q) components



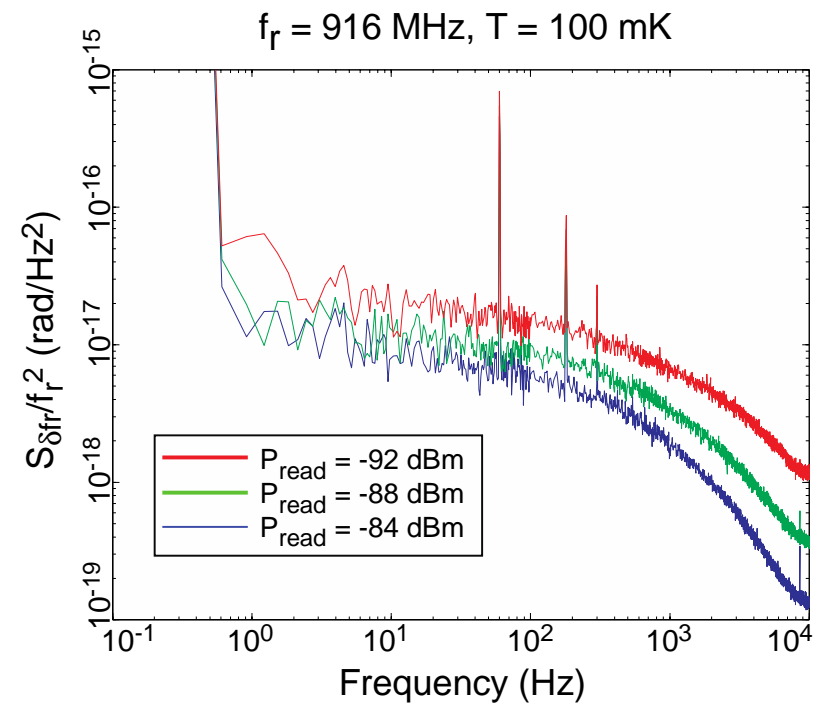
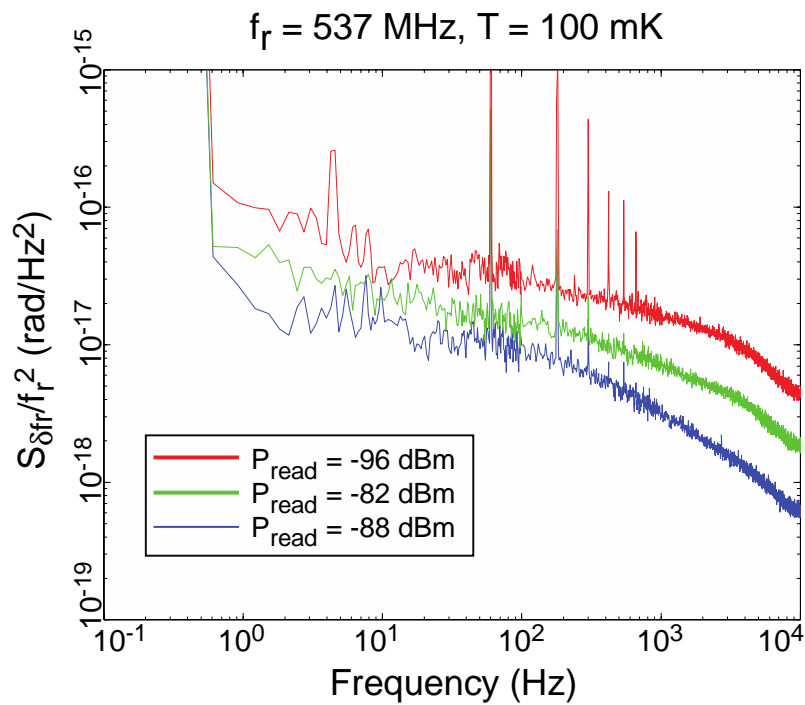
- Decompose noise spectra (S) into parallel and perpendicular components
- Fractional Frequency Noise Spectrum

$$\frac{S_{\delta fr}(\nu)}{f_r^2} = \frac{S_{\parallel}}{16Q^2 r^2}$$

- Our devices – undercoupled ($Q_c/Q_r < 0.05$)
- TLS fluctuations not far above amplifier noise
- Phase noise ~ 2 - 4 x amplifier noise
- Measuring at internal powers not far below critical power in NbTiN

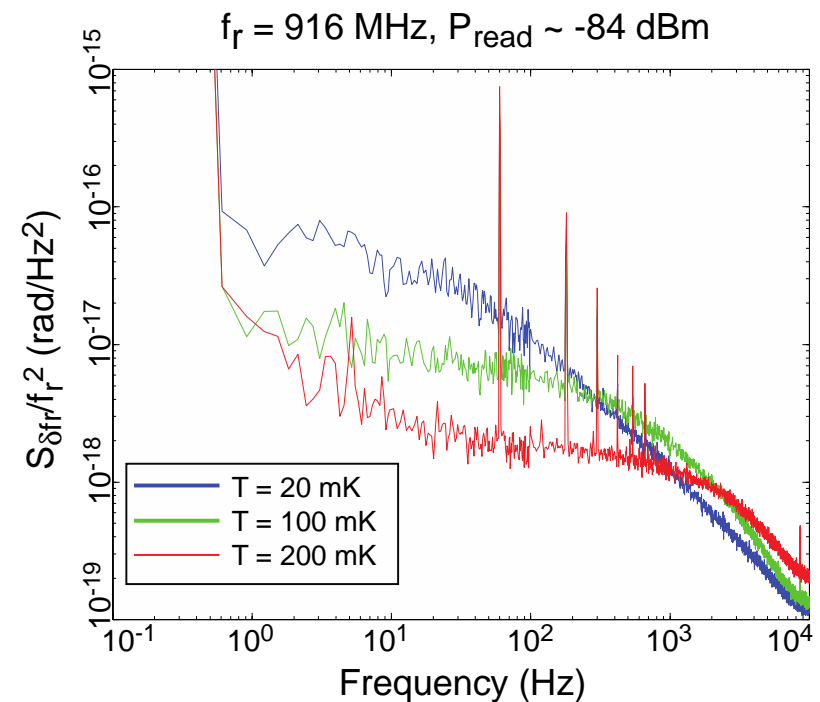
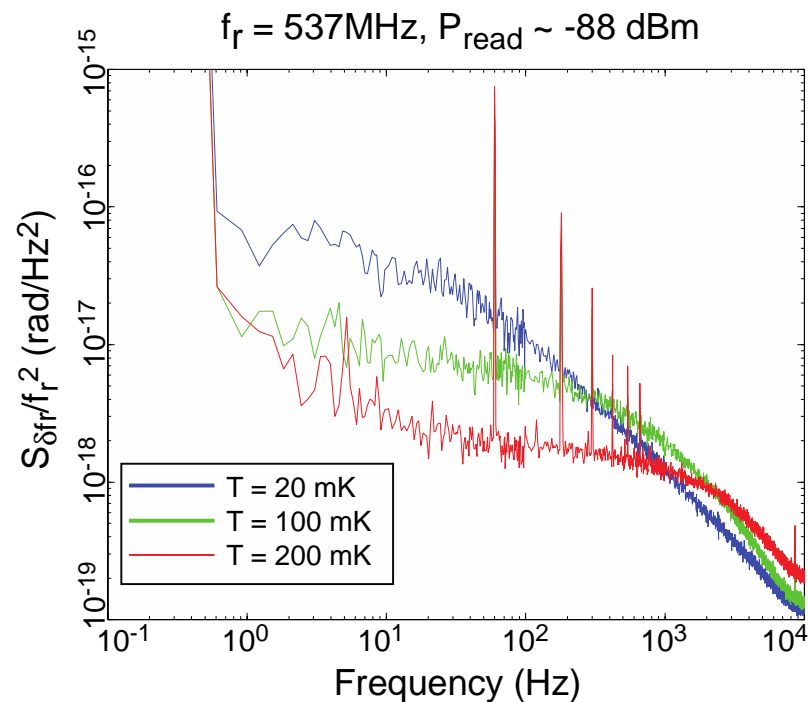
Fractional Frequency Noise Spectra - Power dependence

- Increasing power saturates TLS
- Observe near $P^{-1/2}$ dependence Indicative of TLS
- Observed from ~ 500 MHz – 1 GHz



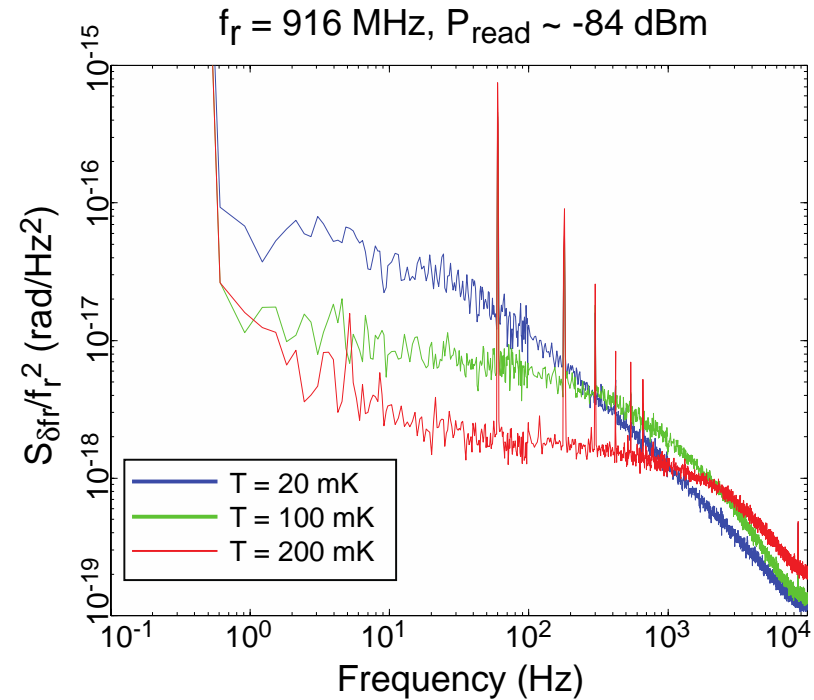
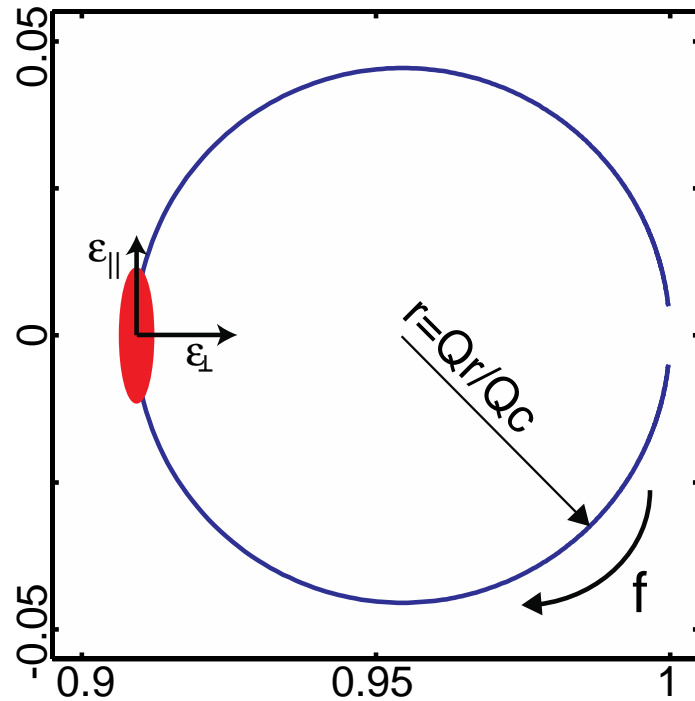
Fractional Frequency Noise Spectra

- Increasing Temperature saturates TLS
- Observe $\sim T^{-2}$ dependence – characteristic of TLS
- Observed from ~ 500 MHz – 1 GHz
- Unusual slope is clear on temperature plot – usually $S_{\text{TLS}} \sim \nu^{-1/2}$



Observed slope deviation from $\nu^{-1/2}$

- Operating about 10 dB below critical current – nonlinearities
- Severely undercoupled
 - Noise is large compared to radius of curvature
 - Phase noise is 2-4x amplifier noise
 - Mixing of I & Q components?



FIR Applications:

- What is the TLS noise under conditions FIR detection?

$$P_{opt} \sim P_{diss}$$

$$P_{opt} = (\hbar \nu_{opt}) \Delta \nu \quad P_{diss} = \frac{\omega_{RF} E_{res}}{Q_i} \quad E = \frac{1}{2} C V^2$$

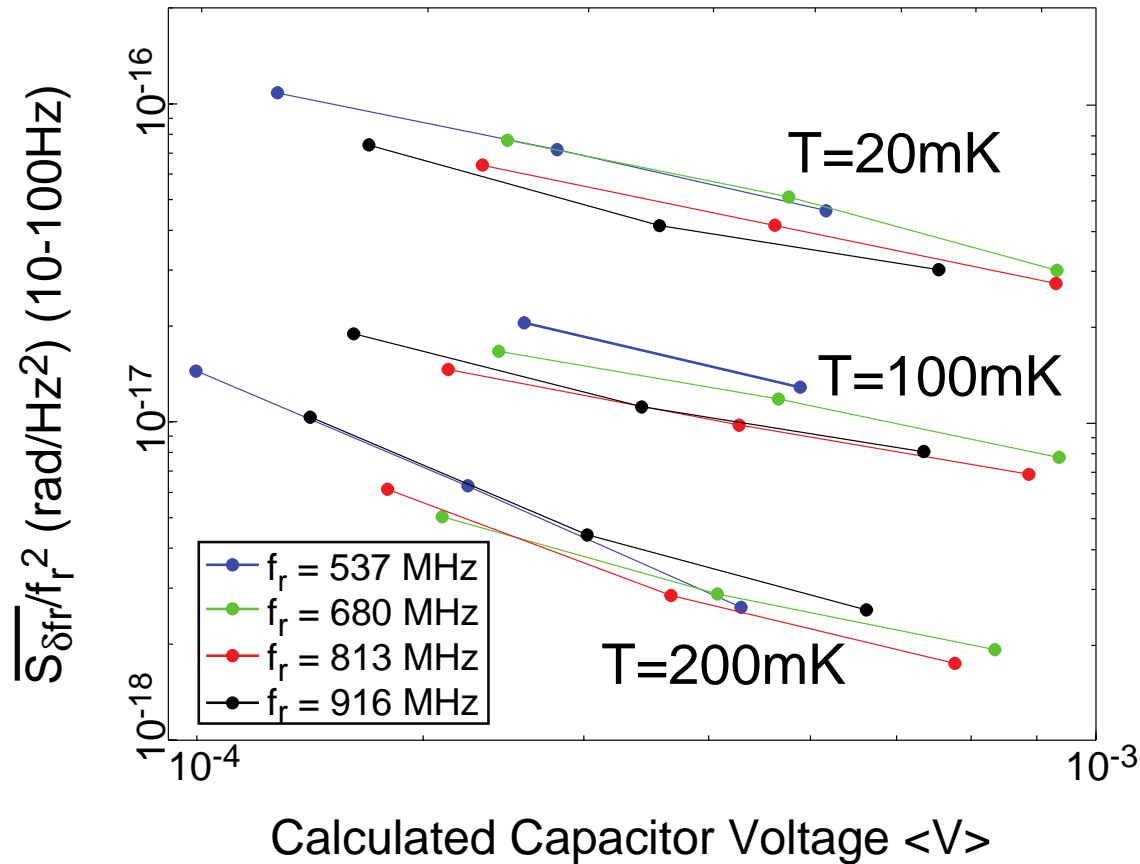
Readout: $Q_i \sim 10^5$, $\omega_{RF} \sim 100$ MHz, $C \sim 10$ pF

Spectroscopy: $\nu = 300$ GHz, $\Delta n = 0.3$ GHz – $V \sim 1.3$ mV

Photometry: $\nu = 300$ GHz, $\Delta n = 100$ GHz – $V \sim 25$ mV

S_{TLS} versus applied voltage to IDC capacitor:

Fractional Frequency Noise



$$\frac{S_{\delta fr, TLS}}{f_r^2} < \frac{\beta^2}{4Q_i^2} \frac{(1+n)}{n\Delta\nu} \sim 10^{-17}$$

Conclusions

Measured TLS noise from 500 MHz – 1 GHz

- TLS noise may be suitable for FIR detection with RF readout schemes
- No clear readout frequency dependence noticed

Remaining goals:

- Measure over wider frequency range and lower powers
 - Improve coupling – measure at lower powers
 - Improve electronics – measure noise at lowest resonator frequencies
- More device geometries: Parallel plate, different size IDC, etc

Thanks

Rick LeDuc

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Peter Day

Loren Swenson

Jonas Zmuidzinas

Kinetic Inductance Thermometry And Radio-Frequency Readouts

Frequency dependence of response
 Mattis-Bardeen: Surface impedance

$$\frac{\sigma_1}{\sigma_N} = \frac{2}{\hbar\omega} \int_{\Delta}^{\infty} dE \frac{E^2 + \Delta^2 + \hbar\omega E}{(\sqrt{E^2 - \Delta^2})\sqrt{((E + \hbar\omega)^2 - \Delta^2)}} [f(E) - f(E + \hbar\omega)]$$

$$\frac{\sigma_2}{\sigma_N} = \frac{1}{\hbar\omega} \int_{\Delta}^{\Delta + \hbar\omega} dE \frac{E^2 + \Delta^2 - \hbar\omega E}{(\sqrt{E^2 - \Delta^2})\sqrt{\Delta^2 - ((E + \hbar\omega)^2)}} [1 - 2f(E)]$$

High Q_i 's and responses possible
 Working at RF makes electronics simpler
 Easily multiplex large number of detectors

